

بِسْمِ اللَّهِ الرَّحْمَنِ الرَّحِيمِ

3D CFD Steady and Unsteady

By:

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Unsteady CFD for 3D problems

- Meshless MFS.
- Fundamental solution for 3D.
- Treatment of domain integral.

Importance of CFD

CFD is an important subject in computational mechanics as the application of fluid dynamics are so many in our life such as:



Flow around buildings

Applications in Biomechanics

Applications in climate problems

Navier Stokes equations

Navier Stokes equations for viscous incompressible flow:

Equation of mass conservation (continuity equ.)

$$\dot{\mathbf{u}}_{i,i}(\mathbf{x}) = 0 \quad i = 1 \rightarrow 3$$

Equation of momentum (dimensionless)

$$-\underbrace{p_{,i}(\mathbf{x})}_{\text{Pressure gradient}} + \frac{1}{Re} \left(\dot{\mathbf{u}}_{i,jj}(\mathbf{x}) + \dot{\mathbf{u}}_{j,ij}(\mathbf{x}) \right) = \underbrace{\dot{\mathbf{u}}_j(\mathbf{x})\dot{\mathbf{u}}_{i,j}(\mathbf{x})}_{\text{Convective term}} + \underbrace{\frac{\partial \dot{\mathbf{u}}_i}{\partial t}(\mathbf{x})}_{\text{Inertia term}}$$

Penalty formulations

Eliminate the pressure term assuming $p(\mathbf{x}) = -\lambda \dot{\mathbf{u}}_{i,i}(\mathbf{x})$

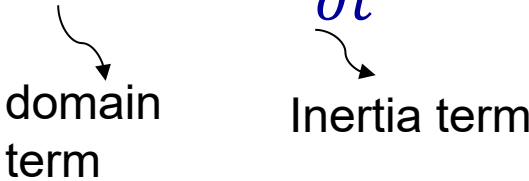
λ must be large enough

Rearranging Navier Stokes equations as follows:

$$\left(\lambda + \frac{1}{Re} \right) \dot{\mathbf{u}}_{j,ij}(\mathbf{x}) + \frac{1}{Re} \dot{\mathbf{u}}_{i,jj}(\mathbf{x}) = \dot{\mathbf{u}}_j(\mathbf{x}) \dot{\mathbf{u}}_{i,j}(\mathbf{x}) + \frac{\partial \dot{\mathbf{u}}_i}{\partial t}(\mathbf{x})$$

Comparing to Navier equation for elasticity:

$$(\lambda + \mu) u_{j,ij}(\mathbf{x}) + \mu u_{i,jj}(\mathbf{x}) = -b_i(\mathbf{x}) + \frac{\partial u_i}{\partial t}(\mathbf{x})$$


domain term Inertia term

The analogy between N-S equations and N equations will be as follows:

$$\dot{\mathbf{u}}_i(\mathbf{x}) \rightarrow u_i(\mathbf{x})$$

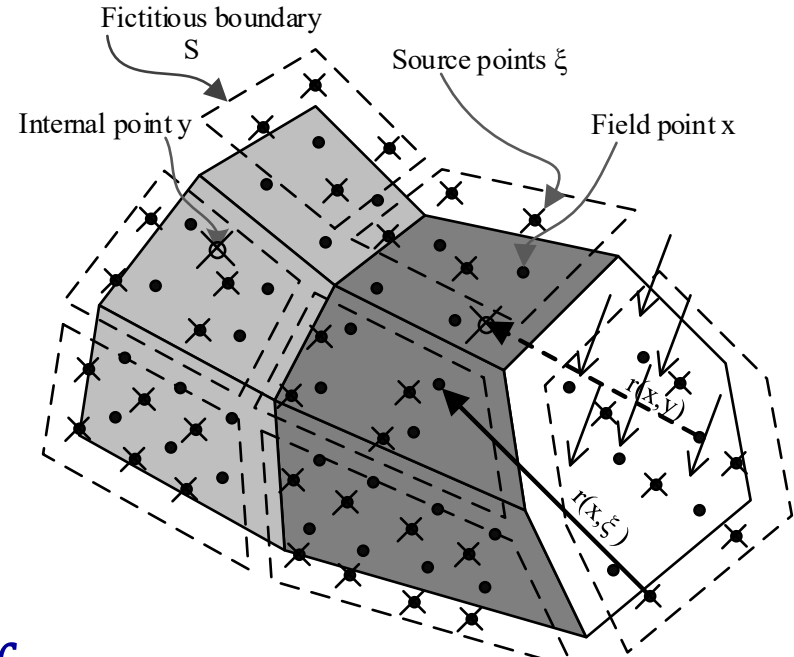
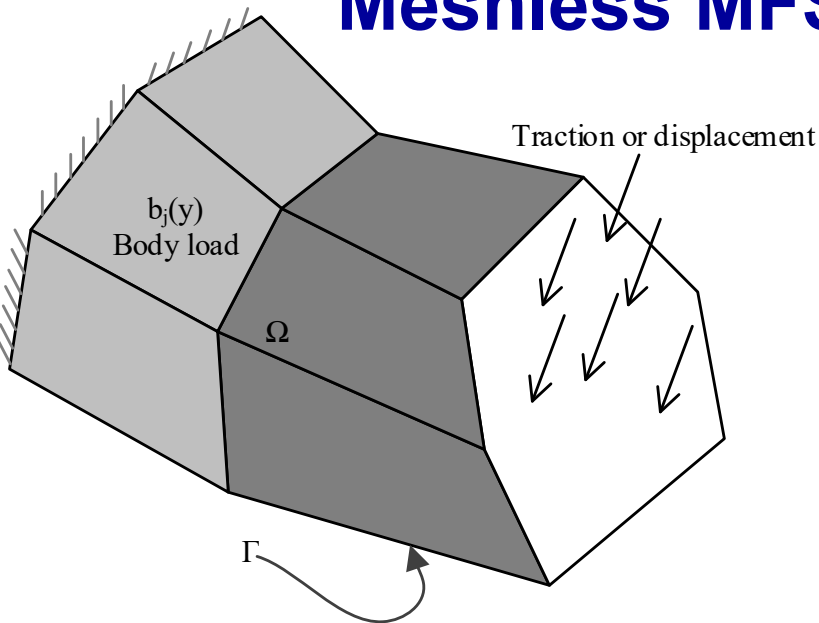
$$\dot{\mathbf{u}}_j(\mathbf{x})\dot{\mathbf{u}}_{i,j}(\mathbf{x}) \rightarrow -b_i(\mathbf{x})$$

$$\frac{1}{Re} \rightarrow \mu$$

$$\lambda \rightarrow \lambda$$

Steady state CFD for 3D problems

Meshless MFS for Single domain



Equation for displacement:

$$u_j(x) = \sum_{k=1}^{k=N} U_{ij}^*(\xi_k, x) \phi_i(\xi_k) + \int_{\Omega(y)} U_{ij}^*(y, x) b_i(y) d\Omega(y)$$

Equation for traction:

$$t_j(x) = \sum_{k=1}^{k=N} T_{ij}^*(\xi_k, x) \phi_i(\xi_k) + \int_{\Omega(y)} T_{ij}^*(y, x) b_i(y) d\Omega(y)$$

The matrix form:

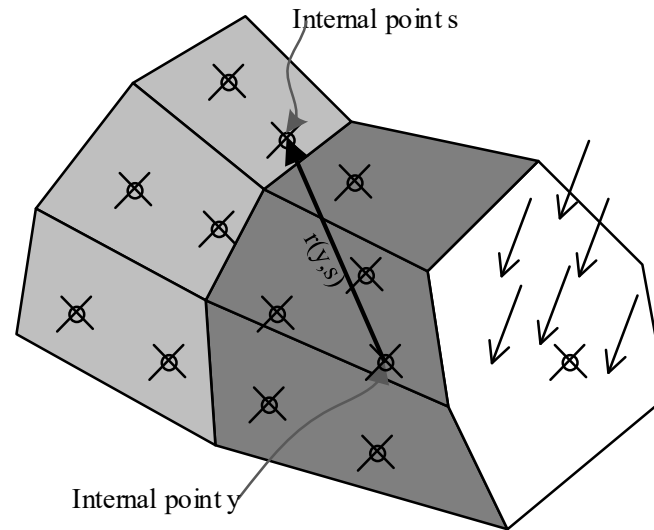
$$\begin{Bmatrix} \{\bar{u}(x)\}_{3N_1 \times 1} \\ \{\bar{t}(x)\}_{3N_2 \times 1} \end{Bmatrix} = \begin{bmatrix} [U^*(\xi, x)]_{3N_1 \times 3N} \\ [T^*(\xi, x)]_{3N_2 \times 3N} \end{bmatrix} \{\phi(\xi)\}_{3N \times 1} + \{b_p(x)\}_{3N \times 1}$$

The convective term calculation:

$$u_{j,m}(s) = \sum_{k=1}^{k=M} U_{ij,m}^*(\xi_k, s) \phi_i(\xi_k) + \int_{\Omega(y)} U_{ij,m}^*(y, s) b_i(y) d\Omega(y)$$

Treatment of domain integral

Using Monte-Carlo integration technique



$$\int_{\Omega(y)} U_{ij}^*(y, x) b_i(y) d\Omega(y) = \frac{\Omega}{N_m} \sum_{m=1}^{m=N_m} U_{ij}^*(y_m, x) b_i(y)$$

Solution procedure:

- Initially compute the matrices .
- Start the loop on the nonlinear term convective terms. compute domain term .
- Solve the system of equations and get ϕ then get boundary velocity and traction.

$$\begin{Bmatrix} \{\bar{u}(X)\}_{3N_1 \times 1} \\ \{\bar{t}(X)\}_{3N_2 \times 1} \end{Bmatrix} = \begin{bmatrix} [U^*(\xi, X)]_{3N_1 \times 3N} \\ [T^*(\xi, X)]_{3N_2 \times 3N} \end{bmatrix} \{\phi(\xi)\}_{3N \times 1} + \{b_p(X)\}_{3N \times 1}$$

- Compute the internal velocity and its derivative.
- Compute the convective term:

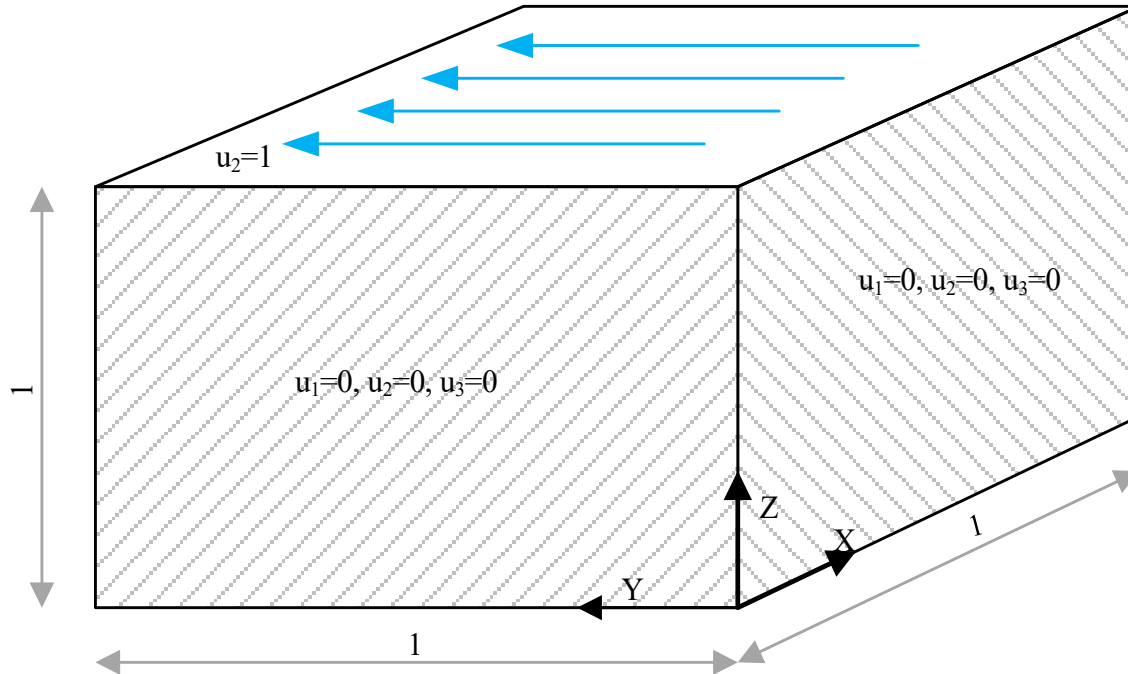
$$b_i(y) = K (b_i(y))^{(l)} + (K - 1) (b_i(y))^{(l-1)}$$

- Compute the difference in results of internal velocities.

$$diff = \frac{(u_j^{(l)} - u_j^{(l-1)}) 100}{u_j^{(l-1)}}$$

Example

Lid driven cavity



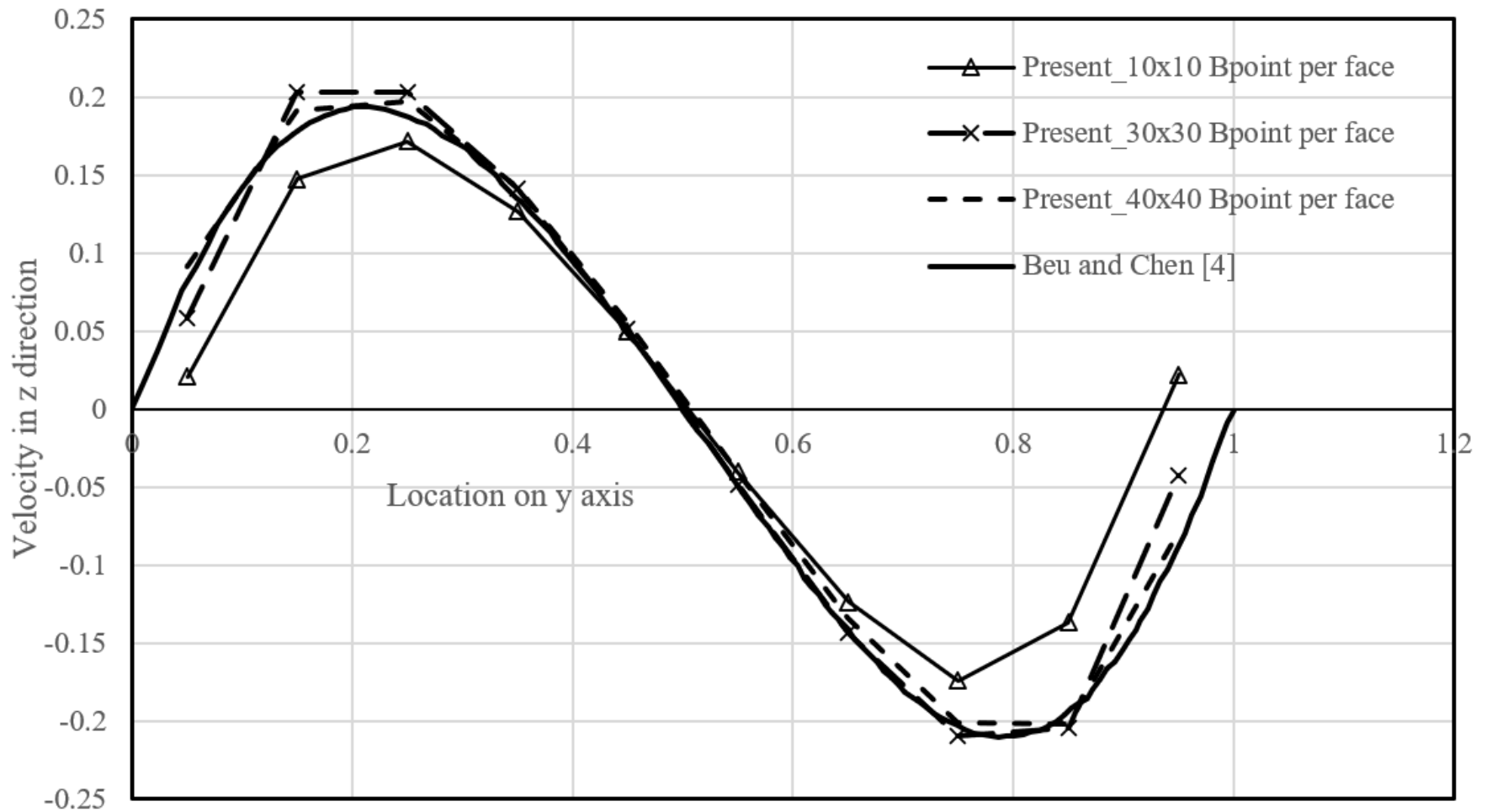
Reynolds number 10 and 100

Poisson's ratio 0.4999999

Relaxation parameter 0.05

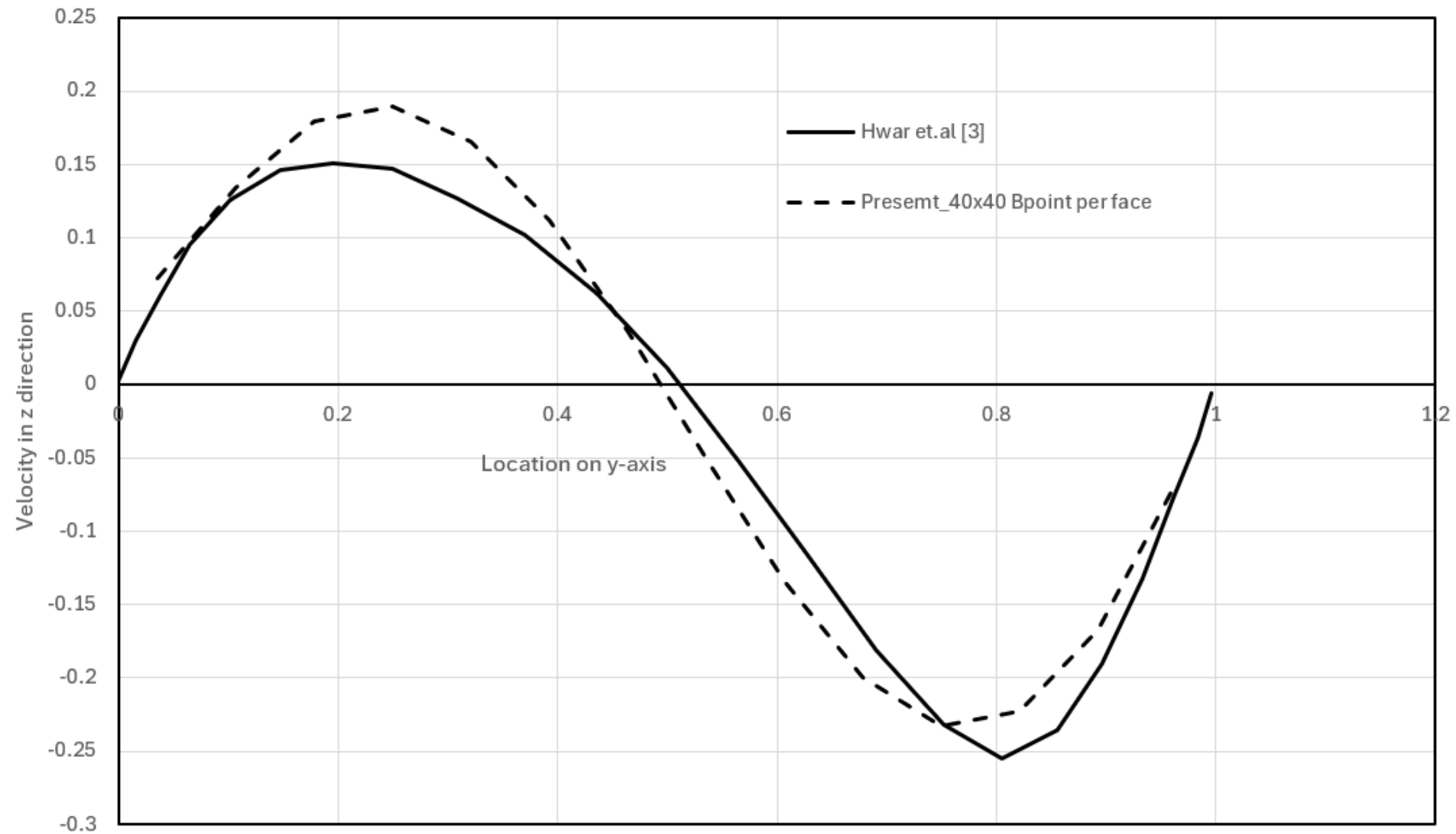
Re 10 with 10x10x10 MC

Offset 100%

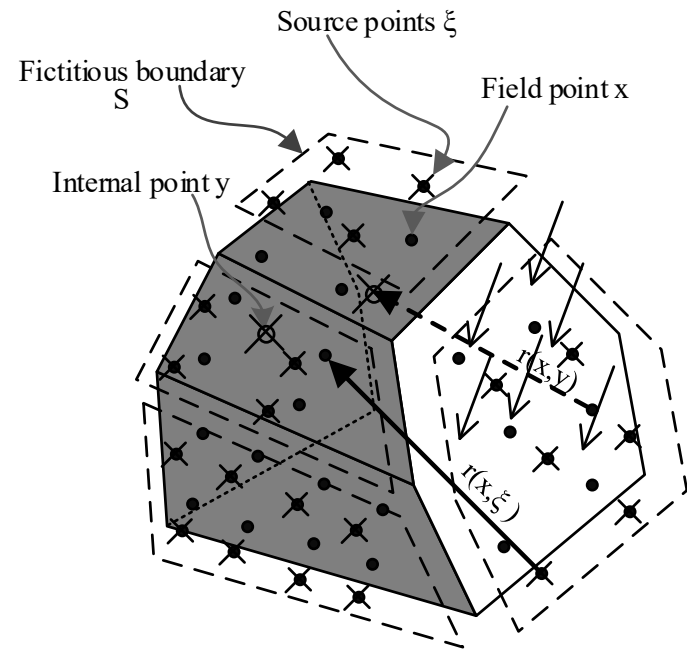
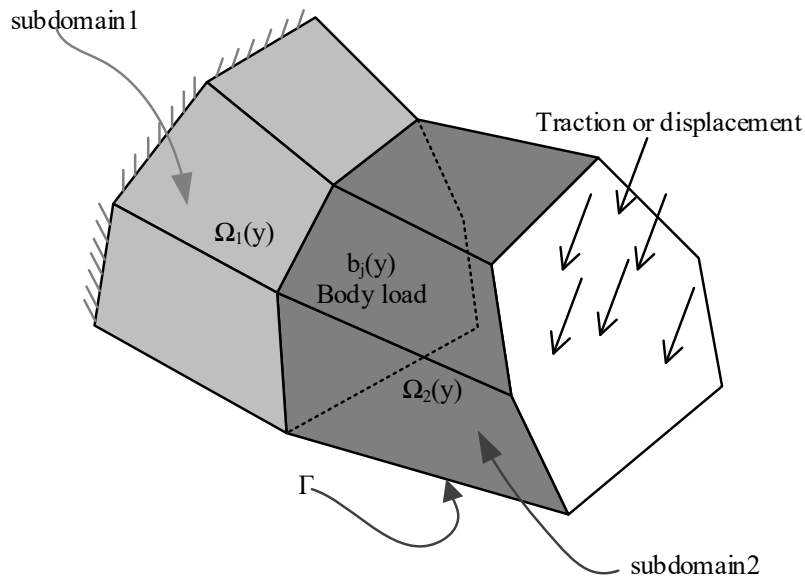


Re 100 with 14x14x14 MC

Offset 300%



Meshless MFS for multi domain



For each sub domain

Equation for displacement:

$$u_j(x) = \sum_{k=1}^{k=N} U_{ij}^*(\xi_k, x) \phi_i(\xi_k) + \int_{\Omega(y)} U_{ij}^*(y, x) b_i(y) d\Omega(y)$$

Equation for traction:

$$t_j(x) = \sum_{k=1}^{k=N} T_{ij}^*(\xi_k, x) \phi_i(\xi_k) + \int_{\Omega(y)} T_{ij}^*(y, x) b_i(y) d\Omega(y)$$

For each subdomain:

$$[F]_{3N_r \times 3N_r} = [K]_{3N_r \times 3N_r} \{u\}_{3N_r \times 1} - [K]_{3N_r \times 3N_r} \{u^p\}_{3N_r \times 1} + [F^p]_{3N_r \times 3N_r}$$

$$[K]_{3N_r \times 3N_r} = [L]_{3N_r \times 3N_r} [T^*]_{3N_r \times 3N_r} [U^*]^{-1}_{3N_r \times 3N_r}$$

Assembly:

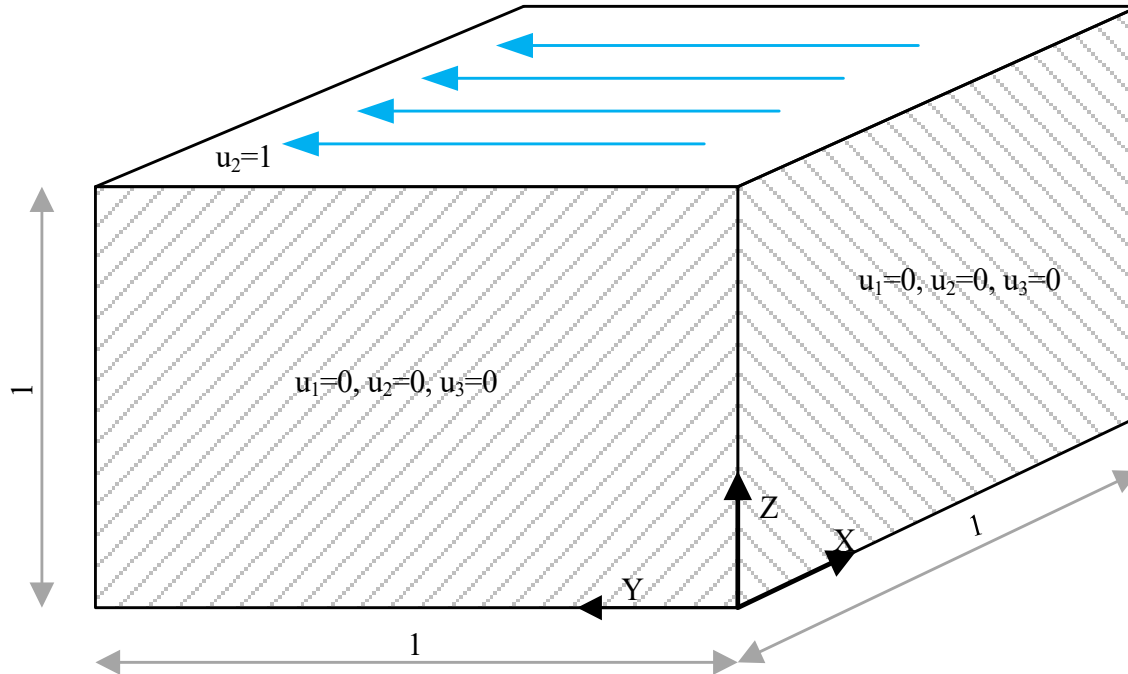
$$\begin{Bmatrix} \{F^N\} \\ \{F^U\} \end{Bmatrix}_{3N \times 1} = \begin{bmatrix} [K_{11}] & [K_{12}] \\ [K_{21}] & [K_{22}] \end{bmatrix}_{3N \times 3N} \begin{Bmatrix} \{u^U\} \\ \{u^N\} \end{Bmatrix}_{3N \times 1} - [K]_{3N \times 3N} \{u^p\}_{3N \times 1} + \{F^p\}_{3N \times 1}$$

Rearrange:

$$\begin{bmatrix} -[K_{11}] & [0] \\ -[K_{21}] & [I] \end{bmatrix}_{3N \times 3N} \begin{Bmatrix} \{u^U\} \\ \{F^U\} \end{Bmatrix}_{3N \times 1} = \begin{bmatrix} -[I] & [K_{12}] \\ [0] & [K_{22}] \end{bmatrix}_{3N \times 3N} \begin{Bmatrix} \{F^N\} \\ \{u^N\} \end{Bmatrix}_{3N \times 1} + \{b^p\}_{3N \times 1}$$

Example

Lid driven cavity

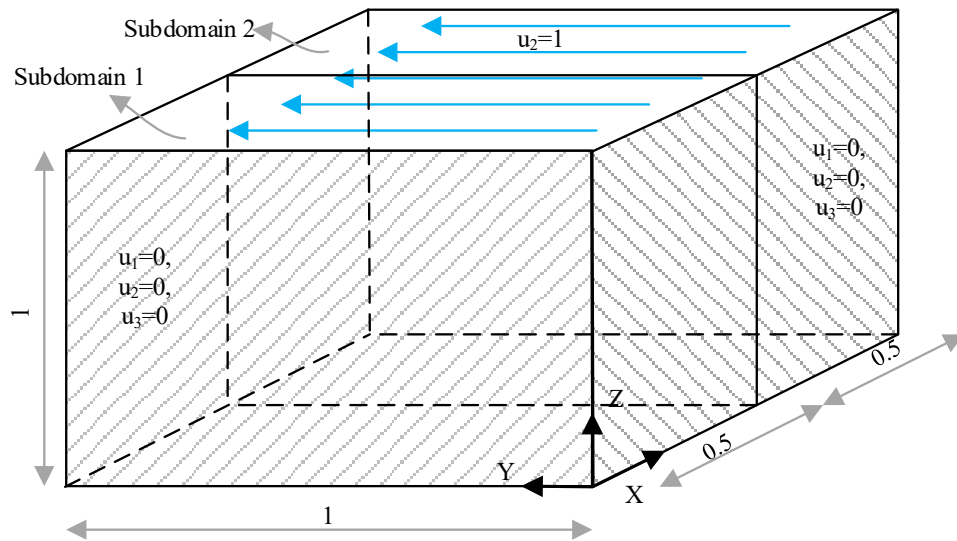


Reynolds number 10 and 100

Poisson's ratio 0.4999999

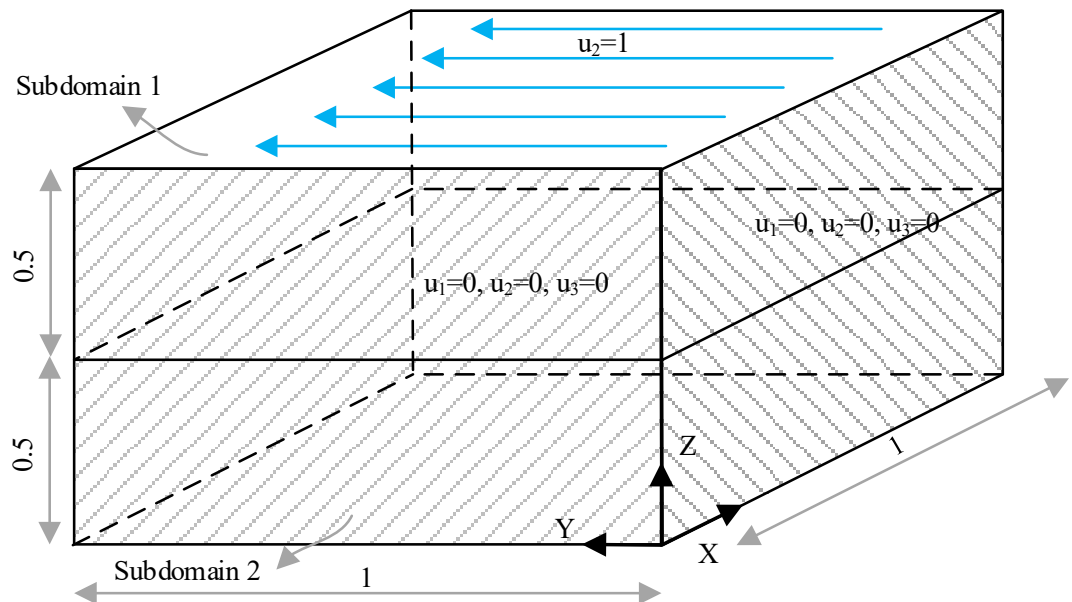
Relaxation parameter 0.05

Example

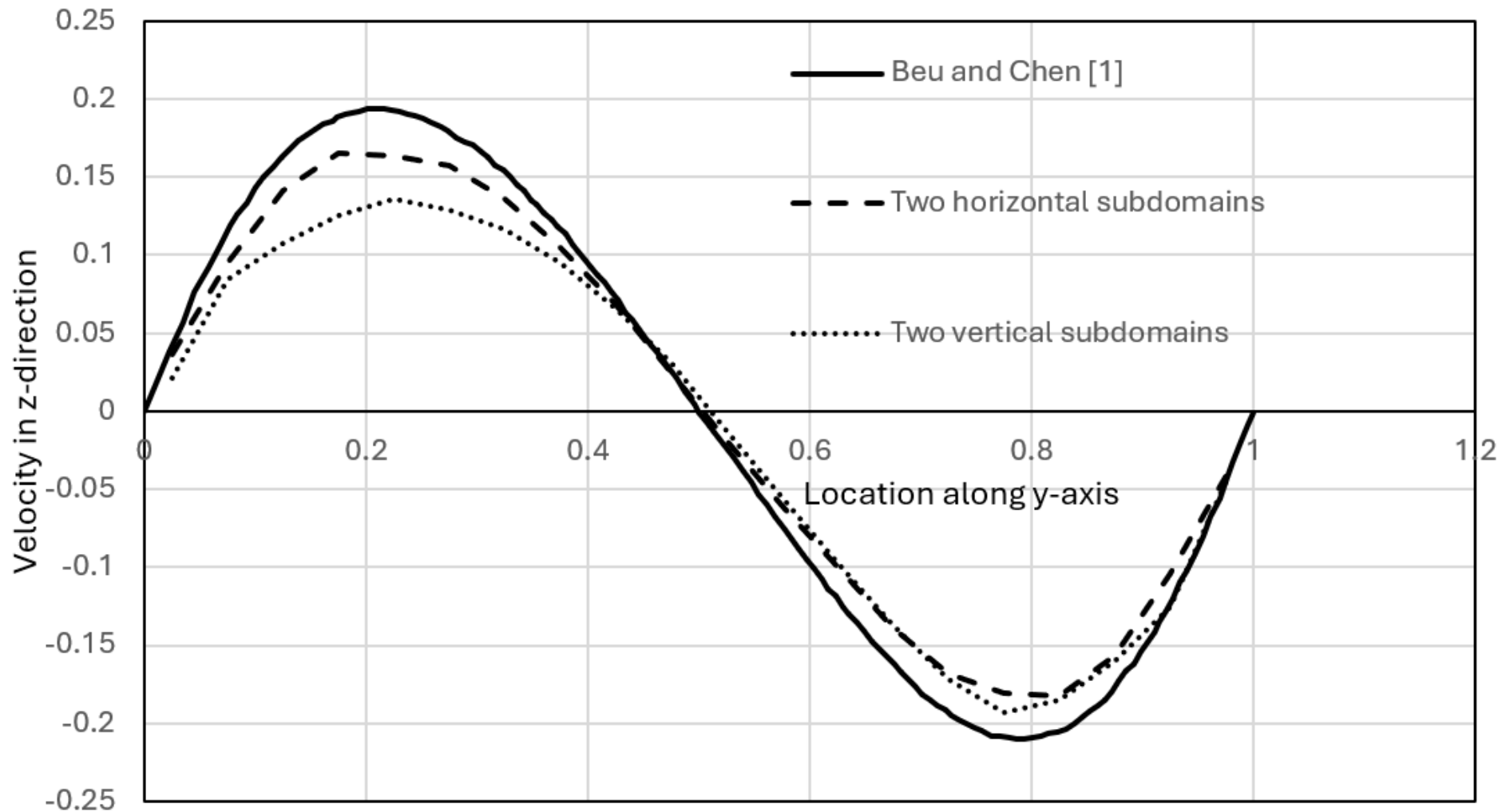


Two vertical subdomain

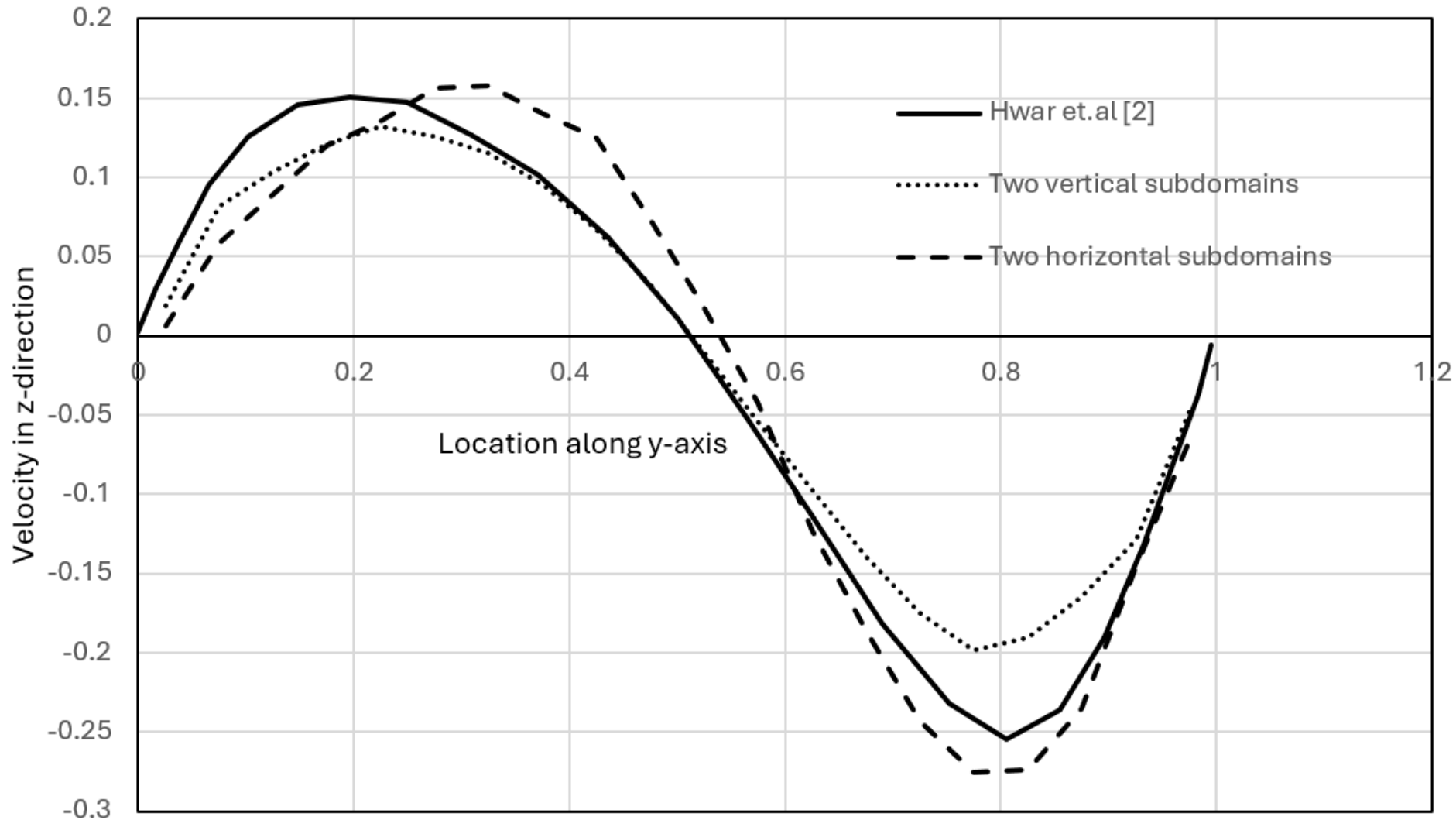
Two horizontal subdomain



Re 10 20x20 BP/face 24x24x24 MC
Offset 0.125 inner and 0.15 outer for the Vert.
Offset 0.21 for the Horz.



Re 100 20x20 BP/face 24x24x24 MC
Offset 0.125 inner and 0.15 outer for the Vert.
Offset 0.21 for the Horz.



Unsteady state CFD for 3D problems

Time differencing technique

The N-S equation at time $t + \Delta t$:

$$(\lambda + \mu)u_{j,ij}^{t+\Delta t}(x) + \mu u_{i,jj}^{t+\Delta t}(x) = -b_i^{t+\Delta t}(x) + \frac{\partial u_i^{t+\Delta t}}{\partial t}(x)$$

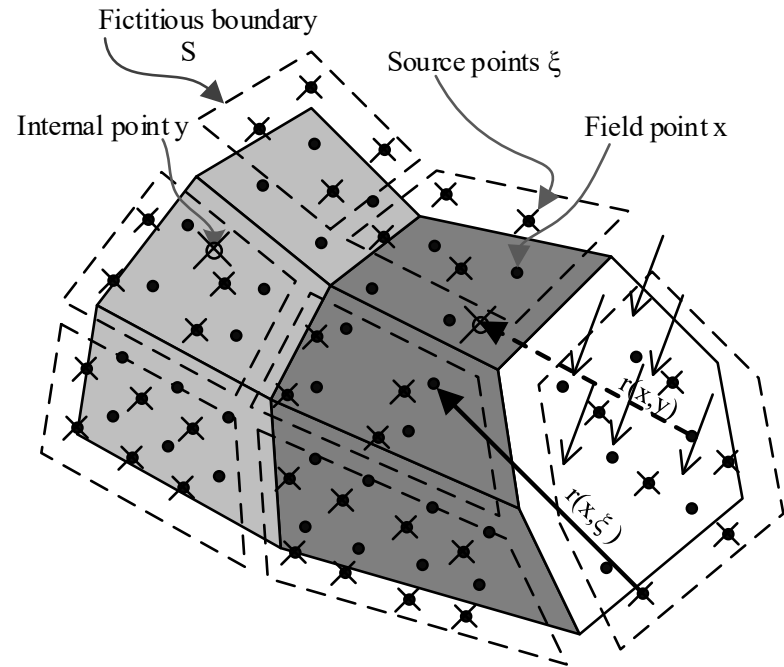
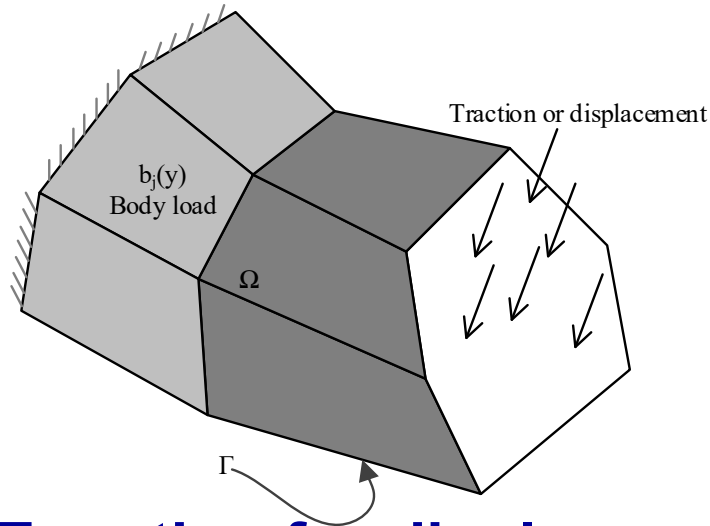
Using Houbolt finite difference scheme:

$$\frac{\partial}{\partial t} u_i^{t+\Delta t} = \frac{11u_i^{t+\Delta t} - 18u_i^t + 9u_i^{t-\Delta t} - 2u_i^{t-2\Delta t}}{6 \Delta t}$$

The governing differential equation can be written as follows:

$$\begin{aligned} L_{ij}u_j^{t+\Delta t}(x) &= -B_i^{t+\Delta t}(x) - b_i^{t+\Delta t}(x) \\ L_{ij} &= \mu \left(\nabla^2 \delta_{ij} + \frac{\partial_i \partial_j}{1 - 2\nu} - \frac{11}{6 \Delta t \mu} \delta_{ij} \right) \\ B_i^{t+\Delta t}(x) &= \frac{18u_i^t - 9u_i^{t-\Delta t} + 2u_i^{t-2\Delta t}}{6 \Delta t} \end{aligned}$$

Meshless MFS



Equation for displacement:

$$u_j^{t+\Delta t}(x) = \sum_{k=1}^N U_{ij}^*(\xi_k, x) \phi_i^{t+\Delta t}(\xi_k) + \int_{\Omega(y)} U_{ij}^*(y, x) \{B_i^{t+\Delta t}(y) + b_i^{t+\Delta t}(y)\} d\Omega(y)$$

Equation for traction:

$$t_j^{t+\Delta t}(x) = \sum_{k=1}^N T_{ij}^*(\xi_k, x) \phi_i^{t+\Delta t}(\xi_k) + \int_{\Omega(y)} T_{ij}^*(y, x) \{B_i^{t+\Delta t}(y) + b_i^{t+\Delta t}(y)\} d\Omega(y)$$

Fundamental solution for 3D

Governing equation

$$L_{ij}U_{jk}^*(\xi, \mathbf{x}) = -\delta(\xi, \mathbf{x})\delta_{ik}$$

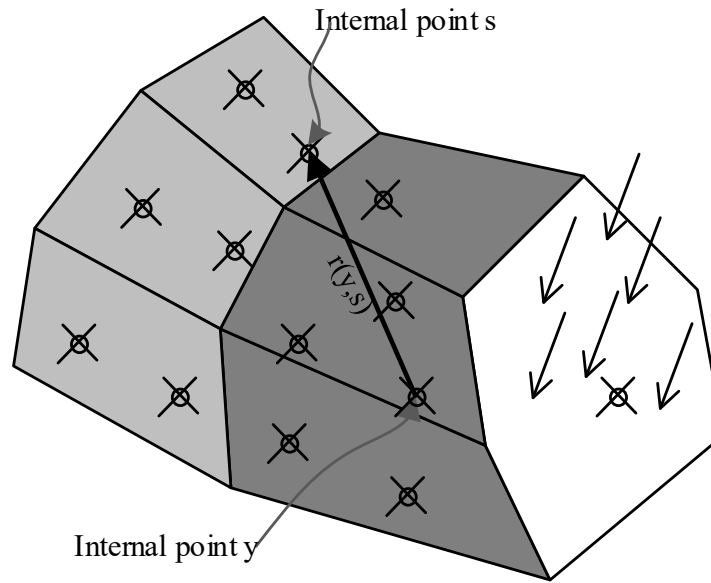
Displacement fundamental solution:

$$\begin{aligned} U_{ij}^*(\xi, \mathbf{x}) &= \frac{-1}{8\pi\mu(1-\nu)(C_1^2 - C_2^2)r^3} \left[\delta_{ij} [e^{-C_1r} - e^{-C_2r} \right. \\ &\quad + r\{C_1e^{-C_1r} - C_2e^{-C_2r} + rC_1^2e^{-C_1r}\}] \\ &\quad + r_{,i}r_{,j} [-3e^{-C_1r} + 3e^{-C_2r} \\ &\quad \left. + r\{-3C_1e^{-C_1r} + 3C_2e^{-C_2r} - rC_1^2e^{-C_1r} + rC_2^2e^{-C_2r}\}] \right] \end{aligned}$$

$$C_1^2 = \frac{11}{6\Delta t\mu} \quad C_2^2 = \frac{1-2\nu}{2(1-\nu)} C_1^2$$

Treatment of domain integral

Using Monte-Carlo integration technique



$$\int_{\Omega(y)} U_{ij}^*(y, x) \{B_i^{t+\Delta t}(y) + b_i^{t+\Delta t}(y)\} d\Omega(y)$$
$$= \frac{\Omega}{N_m} \sum_{m=1}^{m=N_m} U_{ij}^*(y_m, x) \{B_i^{t+\Delta t}(y_m) + b_i^{t+\Delta t}(y_m)\}$$

Solution procedure:

- Initially compute the matrices .

At time step $t + \Delta t$

- Compute the time dependent term from previous velocities at times $(t, t - \Delta t$ and $t - 2\Delta t)$:

$$B_i^{t+\Delta t}(x) = \frac{18u_i^t - 9u_i^{t-\Delta t} + 2u_i^{t-2\Delta t}}{6 \Delta t}$$

- Start the loop on the nonlinear term convective terms. At step l , compute the total domain term .
- Solve the system of equations and get $\phi^{t+\Delta t}$ then get the boundary velocity and traction.

$$\begin{pmatrix} \{\bar{u}^{t+\Delta t}(x)\}_{3N_1 \times 1} \\ \{\bar{t}^{t+\Delta t}(x)\}_{3N_2 \times 1} \end{pmatrix} = \begin{bmatrix} [U^*(\xi, x)]_{3N_1 \times 3N} \\ [T^*(\xi, x)]_{3N_2 \times 3N} \end{bmatrix} \{\phi^{t+\Delta t}(\xi)\}_{3N \times 1} + \{b_p^{t+\Delta t}(x)\}_{3N \times 1}$$

Solution procedure:

- **Compute the internal velocity and its derivative.**
- **Compute the convective term:**

$$b_i^{t+\Delta t}(y) = K \left(b_i^{t+\Delta t}(y) \right)^{(l)} + (K - 1) \left(b_i^{t+\Delta t}(y) \right)^{(l-1)}$$

- **Compute the difference in results of internal velocities.**

$$diff = \frac{\left(u_j^{(l)} - u_j^{(l-1)} \right) 100}{u_j^{(l-1)}}$$

The End

Thanks for your kind attention